

Emission Measurements of an Artificial EUT in an Anechoic Chamber up to 40 GHz

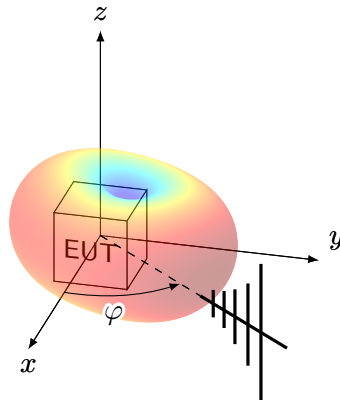
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Chair of Electromagnetic Compatibility
Otto von Guericke University, Magdeburg

September 30, 2024

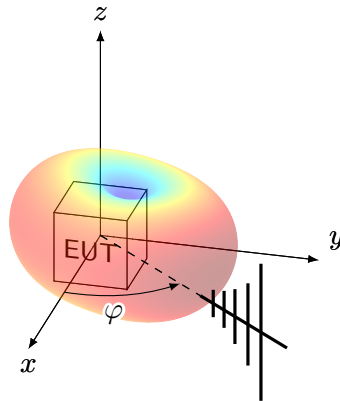
Introduction

- classic focus of EMC - protection of radio communication services
- guaranteed by compliance with emission limits
- verification in fully or semi-anechoic chambers
- spatial sampling of the radiated electric field in the azimuth plane



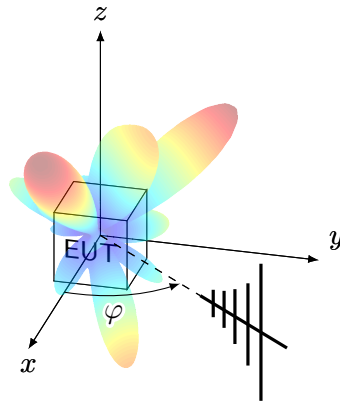
Introduction

- with 5G, some mobile services far above 1 GHz
- existing normative procedures were adopted for frequencies up to 40 GHz
- more complex radiation patterns at higher frequencies
- detecting the maximum becomes less likely



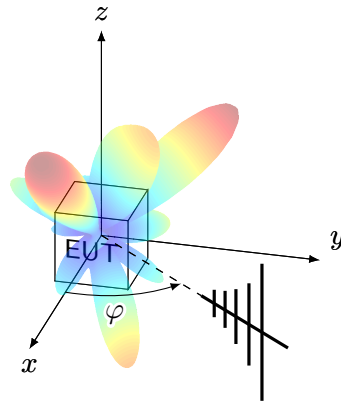
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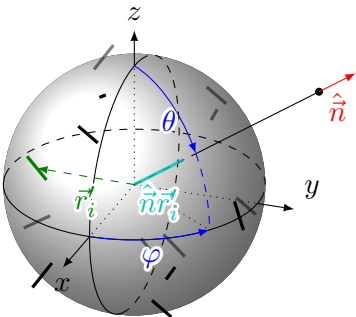
Introduction

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Are the normative methods still suitable?

Stochastic model of a physical unintentional radiator



- small, randomly, oriented and distributed dipole sources
- sphere enclosing EUT
- superposition of far fields
- polarisation effects represented

J. Petzold, et. al. "Monte Carlo Simulation of a Physical Random Unintentional Radiator as a Basis for Statistics in Fully Anechoic Room Measurements," 2023 International Symposium on Electromagnetic Compatibility – EMC Europe, Krakow, Poland, 2023, pp. 1-6



Outline

Artificial EUT

Setup & Procedure

Results & Validation

Conclusion & Outlook



Artificial EUT

Artificial EUT (Front View)

- $310 \times 290 \times 230$ mm (W \times H \times D)
- arbitrarily distributed and oriented slots
- longest slot 75 mm, $f_r = 2$ GHz
- shortest slot 6 mm, $f_r = 25$ GHz



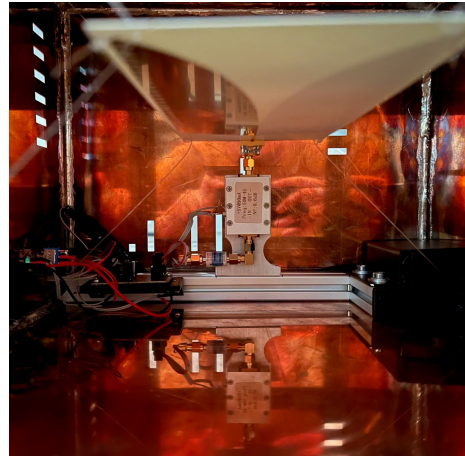
Artificial EUT (Back View)

- $310 \times 290 \times 230$ mm (W \times H \times D)
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Artificial EUT (Interior View)

- 1 GHz sine wave oscillator
- amplifier
- comb generator
- broadband planar vivaldi antenna
- battery powered





Setup & Procedure

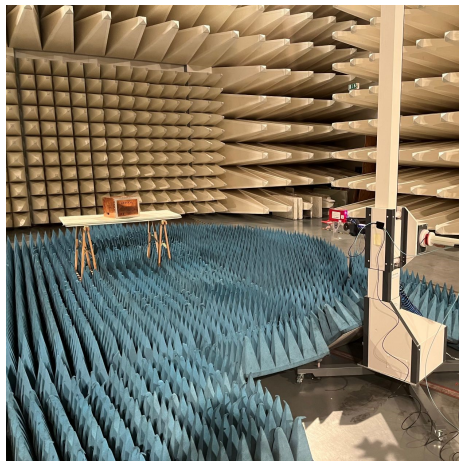
Normative Procedure for Emissions Measurements

Standards

- CISPR-16-2-3 (up to 18 GHz)
- ANSI C63.4-2014 (up to 40 GHz)

General Procedure:

- spatial sampling of the EUT
- horizontal and vertical polarisation
- ANSI: manually position antenna over surface of EUT



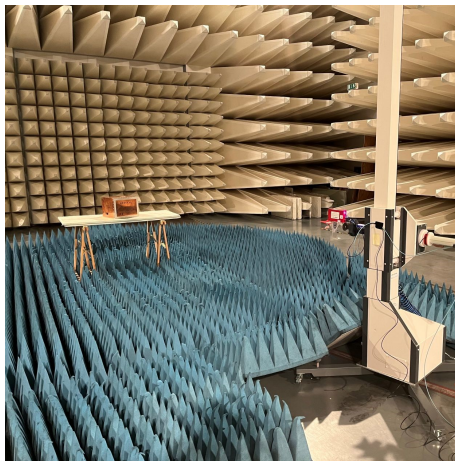
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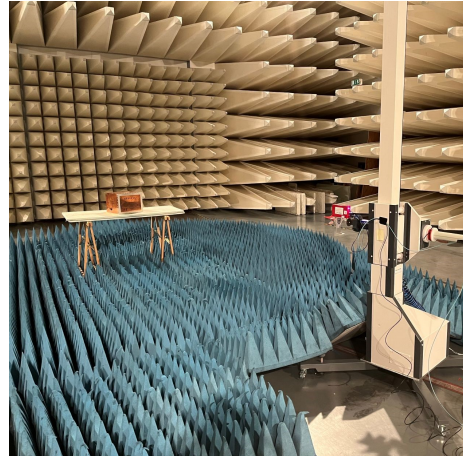
Setup:

- absorber-lined semi-anechoic chamber
- non-conductive table
- turntable and antenna mast



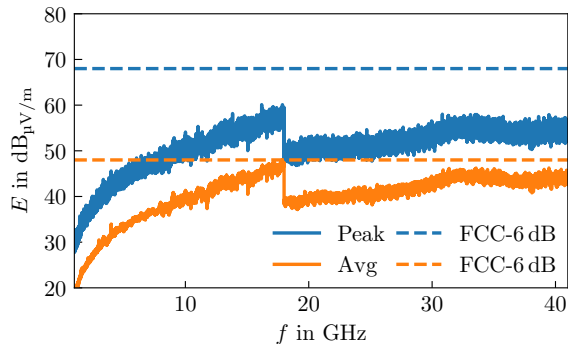
Normative Procedure: Measurement Distance

- preferred measurement distance 3 m



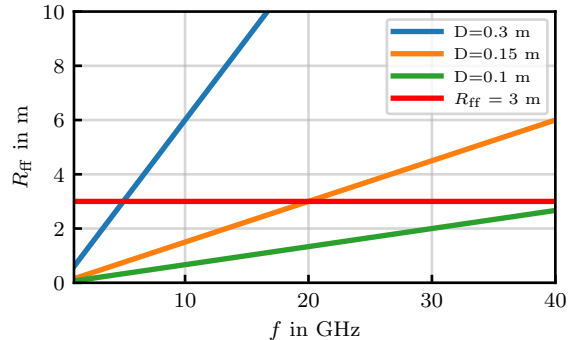
Normative Procedure: Measurement Distance

- preferred measurement distance 3 m
- ambient noise 6 dB below limit



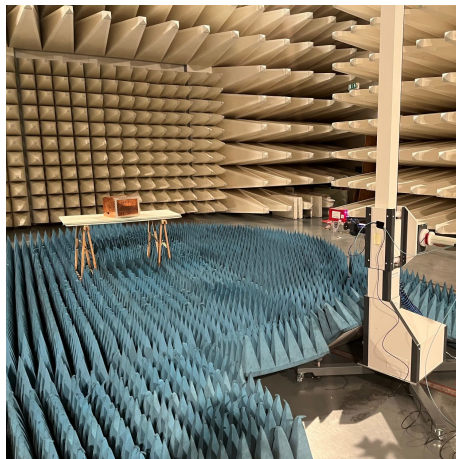
Normative Procedure: Measurement Distance

- preferred measurement distance 3 m
- ambient noise 6 dB below limit
- far field distance $R_{\text{ff}} \approx \frac{2D^2}{\lambda}$



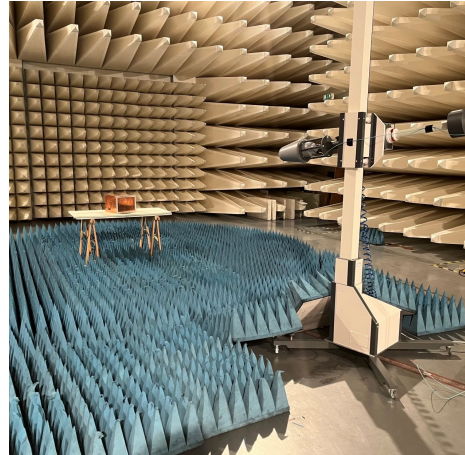
Normative Procedure: Spatial Sampling

- full rotation in azimuth 0° to 360°
- CISPR: $\Delta\phi_{\min} = 15^\circ$
- ANSI: $\Delta\phi_{\min} = 22.5^\circ$
- step size used: $\Delta\phi = 1^\circ$



Normative Procedure: Height Scan

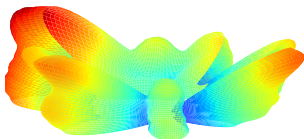
- if beamwidth of antenna smaller than vertical dimension
- 1 m to 4 m (no antenna alignment)
- step size used: $\Delta\phi = 1^\circ$



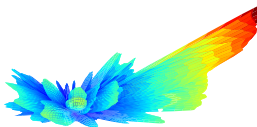


Results & Validation

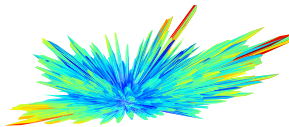
Radiation Patterns



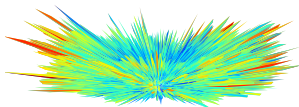
$f = 1 \text{ GHz}, ka = 5, 23$



$f = 6 \text{ GHz}, ka = 31, 41$



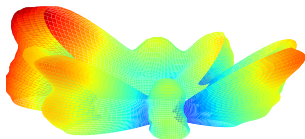
$f = 18 \text{ GHz}, ka = 94, 24$



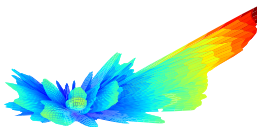
$f = 40 \text{ GHz}, ka = 209, 43$

- lower frequencies, few wide beams
- higher frequencies, many narrow beams
- maximum not in azimuth
- insufficient to determine direction of maximum at one frequency
- despite complexity, many local maxima of same magnitude

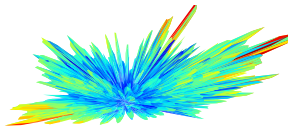
Maximum electric field strength



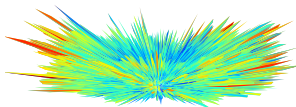
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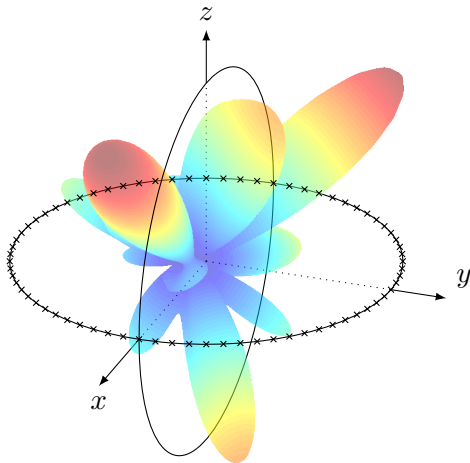


$f = 40 \text{ GHz}, ka = 209,43$

Real detected maximum:

$$E_{\text{real}} = \max_{\varphi, \vartheta} \{E_h(\varphi, \vartheta), E_v(\varphi, \vartheta)\}$$

Maximum electric field strength



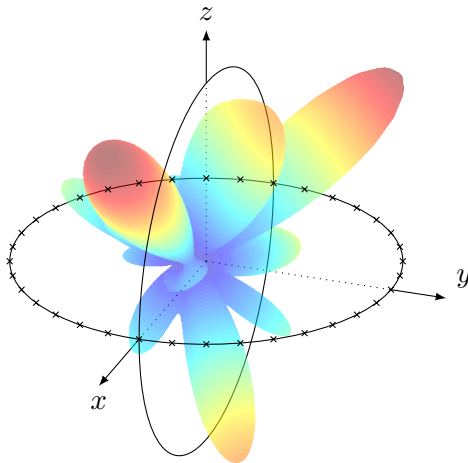
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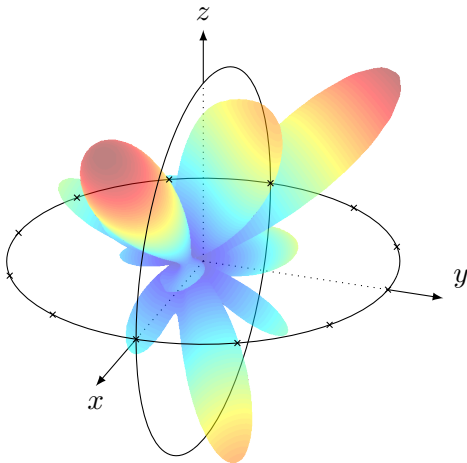
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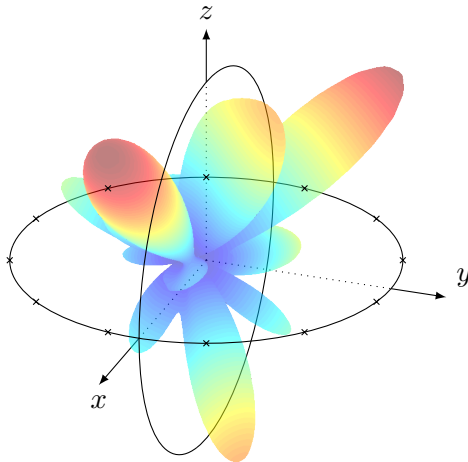
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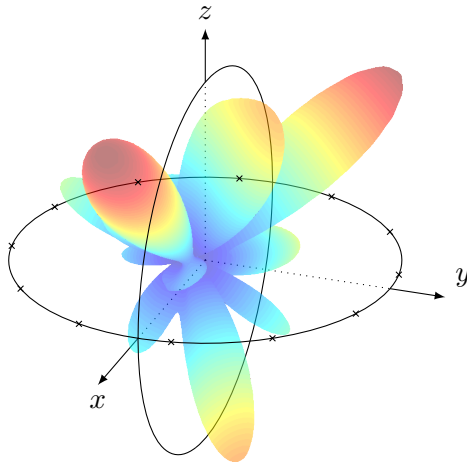
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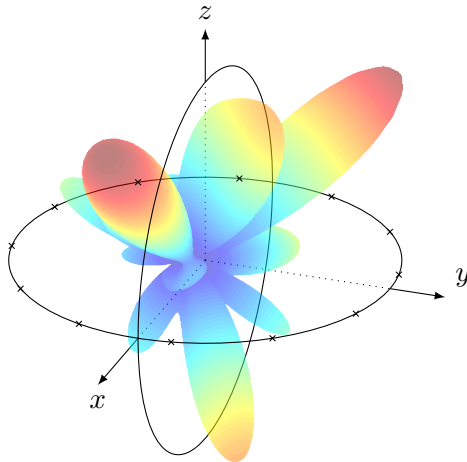
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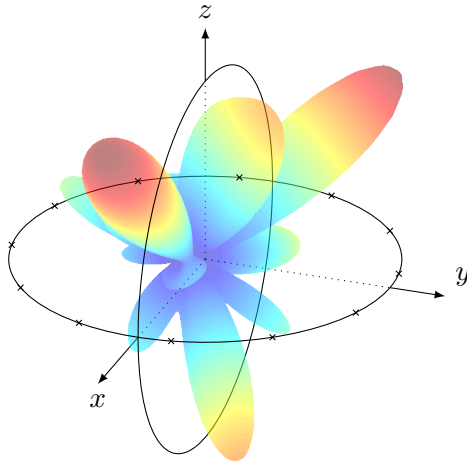
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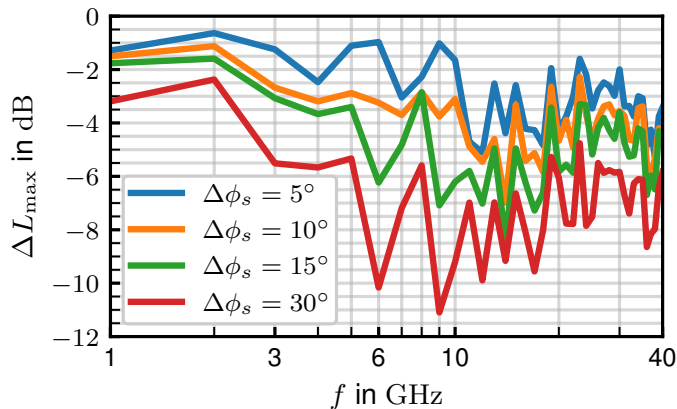
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Relative level difference:

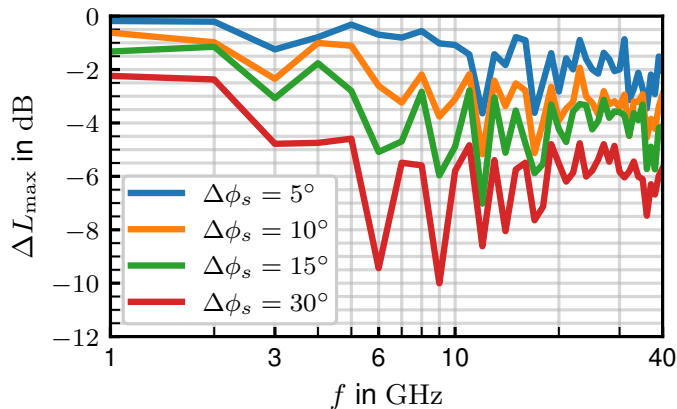
$$\Delta L = 20 \log_{10} \left(\frac{E_{\text{sta}}}{E_{\text{real}}} \right)$$

Influence of the spatial sampling (without height scan)



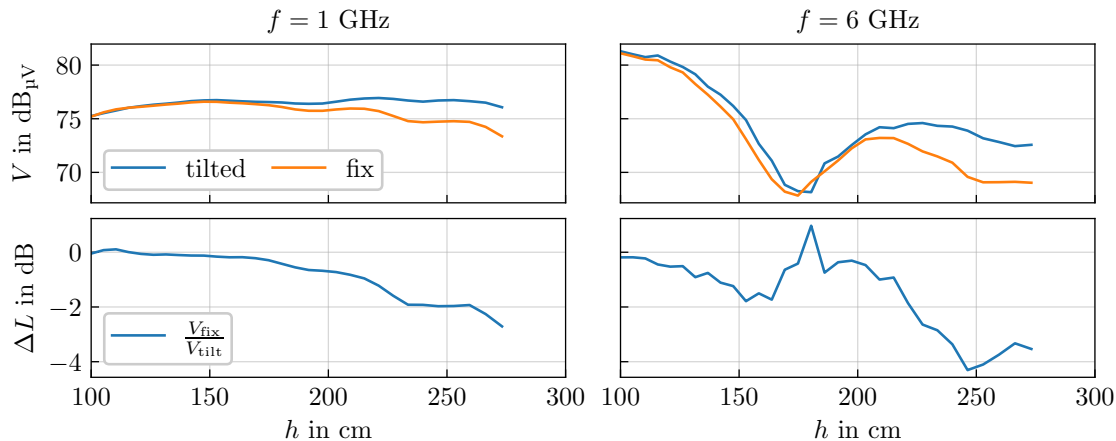
- $\Delta\phi_s \uparrow, \Delta L_{\max} \uparrow$
- $f \uparrow, \Delta L_{\max} \uparrow$
- high $f, \Delta L_{\max} = \text{const.}$

Influence of the spatial sampling (with aligned height scan)

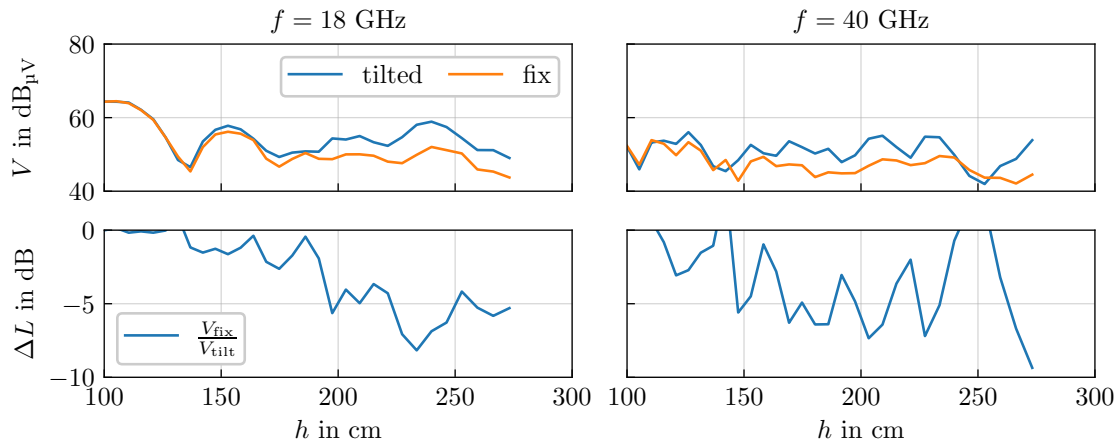


- improvement 2 dB to 4 dB

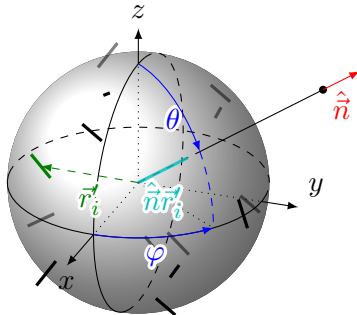
Comparison fixed and aligned height scan



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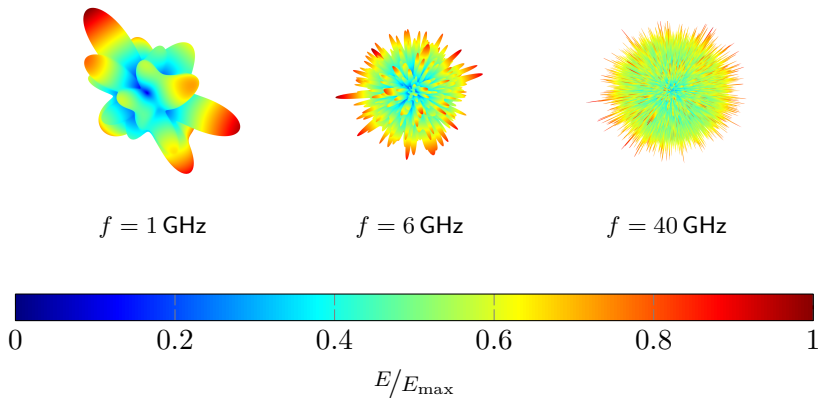
Stochastic model of a physical unintentional radiator



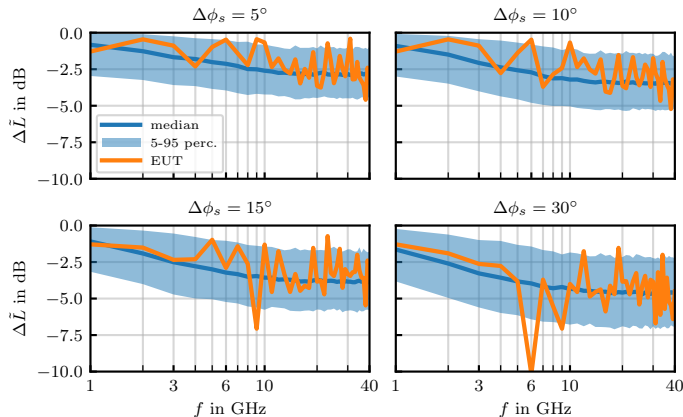
- 50 dipole sources
- radius $a = 24$ cm
- replicate measurements by Monte Carlo simulation
- 1000 realisations

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Radiation Pattern EUT $a = 24$ cm



Validation of the theoretical Model



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$$\Delta L = 20 \log_{10} \left(\frac{E_{\text{sta}}}{E_{\text{real}}} \right)$$



Conclusion & Outlook

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Summary

- Normative procedure is highly dependent on the angular resolution
- For higher frequencies height scan without antenna alignment insufficient
- Stochastic radiator model represents the deviations very well

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- For higher frequencies height scan without antenna alignment insufficient
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Discussion

- Normative procedure not suitable in terms of accuracy and reproducibility
- Definition of a frequency-dependent angular resolution
- Definition of a frequency and angular dependent uncertainty
- Alternative procedure in the mode-stirred chamber according to IEC-61000-4-21

Thank you for your attention!